

**1. Concept of dynamic similarity** (3 points)

For the case of an incompressible flow, assuming the temperature effects are negligible and external forces are neglected, the Navier-Stokes equations consist of conservation of mass

$$\nabla \cdot \mathbf{u} = 0 \quad (1)$$

and conservation of momentum

$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho_0} \nabla p + \nu \nabla^2 \mathbf{u} \quad (2)$$

where  $\mathbf{u}$  is the velocity vector and  $p$  is the pressure,  $\nu$  denotes the kinematic viscosity.

a) Show: The equations (1,2) can be made dimensionless by a length-scale  $L$ , determined by the geometry of the flow, and by a characteristic velocity  $U$ . For example:  $u = U \cdot u_d$ .

Note: the units of  $[\rho_0] = kg/m^3$ ,  $[p] = kg/(ms^2)$ , and  $[p]/[\rho_0] = m^2/s^2$ . Therefore the pressure gradient term in (2) has the scaling  $U^2/L$ .

b) Show: The scalings vanish completely in front of the terms except for the  $\nabla^2 \mathbf{u}_d$ -term! The dimensionless parameter is the Reynolds number and the only parameter left!

*Remark: For large Reynolds numbers, the flow is turbulent. In most practical flows  $Re$  is rather large ( $10^4 - 10^8$ ), large enough for the flow to be turbulent.*

**2. Elimination of the pressure term** (3 points)

Assume a 2D flow without non-linear terms and friction, where the equations reduce to:

$$\rho \frac{\partial u}{\partial t} = -\frac{\partial p}{\partial x} \quad (3)$$

$$\rho \frac{\partial v}{\partial t} = -\frac{\partial p}{\partial y} \quad (4)$$

a) Show: Subtract  $\partial/\partial y$  of (3) from  $\partial/\partial x$  of (4) results in the elimination of pressure.

b) Show: Defining the stream function  $\psi$  through

$$u = -\frac{\partial\psi}{\partial y} \quad ; \quad v = \frac{\partial\psi}{\partial x} \quad (5)$$

(mass continuity being unconditionally satisfied), the incompressible Newtonian 2D momentum and mass conservation degrade into one equation:

$$\partial_t (\nabla^2 \psi) = 0 \quad (6)$$

c) We now consider the rotating framework and add the Coriolis terms  $-\rho f v$  and  $\rho f u$  to the left hand side of (3,4). Subtract  $\partial/\partial y$  of (3) from  $\partial/\partial x$  of (4) to eliminate the pressure terms to derive the vorticity equation! Show that (6) changed into

$$\partial_t (\nabla^2 \psi) + \beta v = 0 \quad (7)$$

### 3. Question about Rayleigh-Bénard instability (2 points)

Describe in words the Rayleigh-Bénard instability. The basic state possesses a steady-state solution in which there is no motion, and the temperature varies linearly with depth:

$$u = w = 0 \quad (8)$$

$$T_{eq} = T_0 + \left(1 - \frac{z}{H}\right) \Delta T \quad (9)$$

When this solution becomes unstable, ... (please continue)

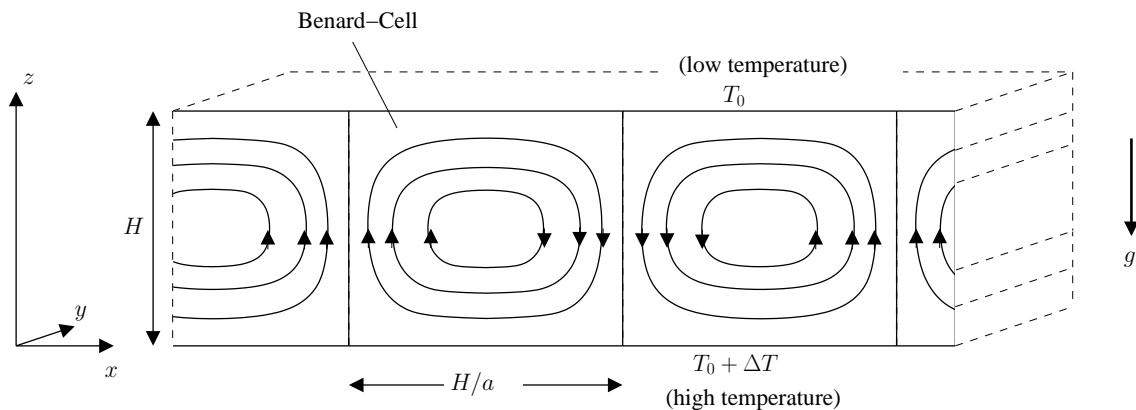


Figure 1: Geometry of the Rayleigh-Bénard system.

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**4. Elimination of the pressure term in the Rayleigh-Bénard system** (3 points)

As above, derive the vorticity equation for

$$D_t u = -\frac{1}{\rho_0} \partial_x p + \nu \nabla^2 u \quad (10)$$

$$D_t w = -\frac{1}{\rho_0} \partial_z p + \nu \nabla^2 w + g(1 - \alpha(T - T_0)) \quad (11)$$

using

$$\partial_x u + \partial_z w = 0$$

$$D_t T = \kappa \nabla^2 T$$

$$T = T_{eq} + \Theta \quad \text{where } \Theta \text{ is the anomaly to the equilibrium solution (9)}$$

For the calculation ignore the non-linear terms.

Show in analogy to (7)

$$D_t (\nabla^2 \Psi) = \nu \nabla^4 \Psi - g\alpha \frac{\partial \Theta}{\partial x}$$

5. **Graphical method for bifurcations** (3 points)

We introduce a graphical method to obtain stability or instability. Consider the "saddle-node bifurcation", one of the equilibrium points is unstable (the saddle), while the other is stable (the node). In Fig. 2, we can plot  $\frac{dx}{dt} = f(x)$  dependent on  $x$  (left panel) for

$$\frac{dx}{dt} = b + x^2 \quad (12)$$

with  $b < 0$  in this particular case (For  $b > 0$  we would have no equilibrium, and we have no point  $x_e$  with  $f(x_e) = 0$ ). We just consider the slope  $f'(x_e)$  and see that the filled circles with positive slope are unstable, the open circles with negative slopes are stable (right panel in Fig. 2).

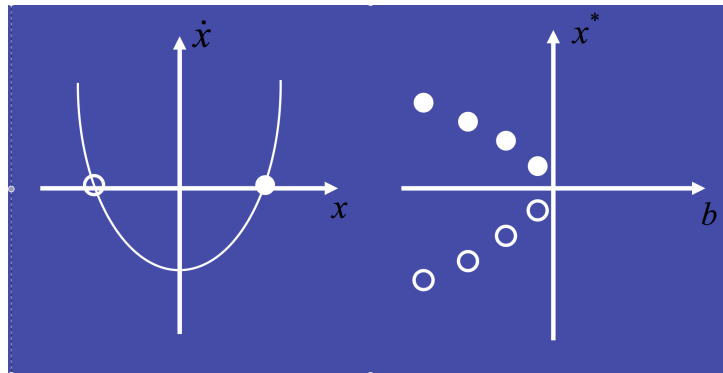


Figure 2: Saddle-node bifurcation diagram using the graphical method.

- (a) Draw the bifurcations as in Fig. 2 for the pitchfork bifurcation.

$$\frac{dx}{dt} = r \cdot x + x^3 \quad (13)$$

- (b) Draw the bifurcations as in Fig. 2 for the transcritical bifurcation.

$$\frac{dx}{dt} = r \cdot x - x^2 \quad (14)$$

Notes on submission form of the exercises: *Working in study groups is encouraged, but each student is responsible for his/her own solution. The answers to the questions can be send until the due date (12:00 pm) to Alessandro Gagliardi (Alessandro.Gagliardi@awi.de), Georg Huettner (Georg.Huettner@awi.de).*